

A NEW VACUUM-TUBE **VOLTMETER**

• THE TYPE of peak-reading vacuum-tube voltmeter now considered standard in the communications industry was first introduced by the General Radio Company some ten years ago when the Type $726-A$

Vacuum-Tube Voltmeter was announced.¹ The novel design and excellent performance of this voltmeter has maintained its popularity over the intervening years considerably beyond the time when advances in the art would normally necessitate a new design. The development, during this period, of new tubes, circuits, and construction techniques has, however, progressed continuously, and these now make it possible to design a completely new instrument having even better performance.

In the design of the new Type 1800-A Vacuum-Tube Voltmeter, which replaces the Type 726-A, effort has been directed to correcting the minor disadvantages that have been found in the older voltmeter as well as to incorporating desirable new features that make the instrument more flexible and convenient.

¹W. N. Tuttle, "Type 726-A Vacuum-
Tube Voltmeter," General Radio Experimenter, Vol. XI, No. 12, May 1937, menter,
pp. $1-6$.

Figure 1. Panel view of the Type 1800-A Vacuum-Tube Voltmeter.

Some of these disadvantages were:

1. The shielding of the probe of the Type 726-A was not complete, and trouble with pickup from strong fields at frequencies over about 50 Mc was sometimes encountered.

2. Individual zero adjustments for each range were used in the Type 726-A, and these sometimes drifted from their correct setting, so that readjustment of the zero when switching from range to range was necessary.

3. The voltage-regulating transformer in the Type 726-A was explicitly designed for one line frequency. In addition, the transformer radiated an appreciable 60-cycle field.

4. The Type 726-A probe was relatively bulky and difficult to get into confined spaces.

5. The Type 726-A meter was somewhat difficult to read at a distance because of the knife-edge pointer and was confusing because of the arrangement of the scales. Reflections from the glass were often bothersome, and the light from the pilot light distracting.

6. The cabinet of the Type 726-A, while convenient for ordinary bench use, was rather large and could not readily be used in other positions than the normal one in which the panel was at a 15° angle to the horizontal.

These disadvantages, with others of a more minor nature, have all been eliminated in the Type 1800-A, and many new features have been added. These include:

1. The natural frequency of the probe has been increased by nearly 3:1, and the gain in high-frequency performance because of the complete shielding is even greater.

2. The input capacitance has been reduced by a factor of 2, and the parallel resistance component increased fourfold at low frequencies.

3. An additional 0-0.5 volt scale has been added that extends the sensitivity by a factor of 3.

4. A complete set of d-c scales has been added, covering the same ranges as the a-c scales.

5. A set of terminal parts has been provided that makes it possible to assemble, on the end of the probe, connectors that will fit all standard General Radio Type 138, 274, and 774 terminals.

6. The new instrument is smaller, lighter, and easier to use.

7. It can be operated with the panel horizontal, vertical, or inclined.

METER

Figure 2 shows the arrangement of the five scales on the face of the meter. The two outer scales, 0 to 15 and 0 to 5 . are linear. On these two scales are read all d-e voltages and all a-c voltages above 5 volts. The non-linear inner scales, 0 to 0.5, 0 to 1.5, and 0 to 5, are used only for a-c voltage measurements of 5 yolts or less. The a-c scales are calibrated to read the r-m-s value of a sinewave voltage or 0.707 times the peak value of a voltage of complex wave shape. The accuracy of all d-c ranges and all a-c ranges at low frequencies is \pm 2% of full scale.

A mirror has been located between the inner and outer groups of scales. The mirror, of course, does not increase the accuracy of the voltmeter, but it does make it possible to read a voltage more precisely than when no mirror is present. The extra precision of reading or setting is most important when small differences must be observed. Without a mirror, parallax makes it very difficult to observe small movements of the pointer, especially when the attention of the observer must be removed momentarily from the meter to some part of the circuit under test. With a mirror,

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tbe eye can be placed precisely over the pointer for every reading. The upper portion of the pointer has been made knife-edged to facilitate further the precise observation of small differences. The lower portion has been made broad so that the approximate position of the **pointer can be seen from some distance away.**

Quite often small differences must be observed in an a-c voltage that is not properly read on one of the linear scales under the knife-edged portion of the pointer. If the voltage is above approximately 0.5 volt, the difference can be observed on the corresponding linear scale with only a small error. If the voltage is less than approximately 0.5 volt, the difference read on the linear scale must be corrected for the nonlinearity of the a-c scale. Of course, the actual voltage level, if it must be known, should be read on the correct a-c scale.

The meter face is illuminated by two lamps inside the meter case. The illu**mination makes a pilot light unnecessary** and **eliminates** bothersome reflections f **from** the glass over the meter face.

PANEL

On the panel, in addition to the m **are input terminals** for a -c **and d-c voltage measurements, and three operating controls. The panel is shown in Figure 1. The d-c terminals, at the**

Figure 2. Close-up of the meter scales. The legend at the left is carried to the top two scoles by a line that, in thi5 view, is hidden by the meter case.

upper left, provide two different input impedances. The input resistance at thc vertical pair is 10 megohms, while the horizontal pair apply the voltage directly to thc grid of thc d-c amplifier tube. A link is provided to short-circuit the pair of terminals not being used. The a-c terminals, which can be used only when the probe is plugged into its position behind the panel, are at the upper right. The LOW terminal is not grounded directly to panel but is isolated by a blocking condenser. A shortcircuiting link is provided to ground the LOW terminal if it is desired to do so. Internal connections for a-c or d-c voltage measurement are made by the combined power and selector switch located at the left under the meter.

The center knob operates the VOLTAGE RANGE selector switch, which is used to select the appropriate voltage range for either a-c or d-c **measurements. The zero control is oper**ated by the knob at tbe right. The zero setting is not changed by operation of the VOLTAGE RANGE switch, although slight readjustment may be required when the $A-C$ $-D-C$ switch is operated. The line fuses, located at the bottom of the panel, can be replaced $with the aid of a screwdriver without$ **removing the instrument from its** cabinet.

CABINET

The shielded walnut cabinet is pro**vided with a storage compartment at** the top for the probe and the various **terminals** supplied. Figure 3 is a view of the compartment with the probe **plugged into position to allow use of the panel a-c input terminals. There to; a** slot in each side of the cabinet for passage of the probe cable when the probe is used externally and the compartment cover is closcd. The two slots **have proved to be very convenient** when the probe must be used at some distance from either side of the instrument.

The voltmeter can be used without separate support in any one of three **positions: vertical, horizontal, and in**clined. The three positions of use, together with the small size and light

Figure 4. Exploded view of the probe and the various terminal finings.

Figure 3. View of the storage compartment at the top of the cabinet. The probe fittings are stored here. The preliminary model used for this photograph has only one slot for the probe cable. Final models have a slot on each side of the cabinet.

weight, make the instrument easy to use in practically any set-up.

In an inclined position, the instrument is supported by the metal carrying handle at an angle of approximately 30 degrees from the horizontal. The handle locks automatically either in the vertical **position, Le., parallel to the panel, or in** the horizontal position. It is released mercly by pressing in on the handle near each hub.

PROBE CIRCUIT

The a-c input voltage is rectified by a diode, which, at input voltages over 5 volts or so, gives a linear d-c voltage output very nearly equal to the peak value of the a-c input voltage. At lower voltages, the d-c voltage output tends to vary as the square of the a-c input **voltage. Therefore, non-linear scales are needed for measurement of a-c voltages** up to 5 volts.

The tube chosen for use as the diode rectifier is the Type 9005 acorn tube. The 9005 was chosen because its natural frequency of 1500 megacycles is the highest of any diode commercially avail-

able. Because of great carc taken in the design of the probe containing the diode and the associated circuit elements (Figure 4), the resonant frequency of the probe input circuit has been kept at 1050 megacycles $-$ two-thirds as high as the resonant frequency of the tube itself. The high resonant frequency was obtained by making the probe small and compact and by minimizing the length of all input connections. The plate of the diode is coupled directly to the high input terminal by a buttontype condenser, and the cathode of the diode is connected to the probe shell by a very short eonnecting strip.

The resonant frequency of 1050 megacycles makes it possible to measure voltages over a wide frequency range without applying corrections. Up to 300 **Me, for instance, the maximum error is** $\pm 12\%$ when the indicated voltage is 0.5 volt or more. If the indicated voltage is less than 0.5 volt, the error will be larger because of the increase of the transit-time error of the diode. In Figure 5 are shown curves from which

corrections for frequency error can be obtained. The curves show that the fre**quency error caused by input circuit resonance is in the opposite direction from the transit-time frequency error.** For instance, at 0.5 volt indicated, the **correction for transit-time balances the** correction for resonance at 500 Mc and the net error is zero. When accurate **measurements are not necessary, the** instrument can be used as a voltage indicator up to 2500 Mc.

Figure 5. Frequency correction fOf' a number of different indicated voltages. The curve marked co is included to show the complete resononce effect.

The transit-time (or premature-cutoff) error varies directly with the interelectrode spacing and would, therefore, be less with a tube having more closely **spaced elements. The spacing, however,** is only a few thousandths of an inch, and **it seems impractical to decrease this** spacing without lowering the voltage rating to a point where the high-voltage **limit would be too low for an instrument** designed to respond to voltages up to 150 volts.

An inspection of the curves makes it clear that the premature cutoff, in general, contributes substantial errors at all voltages at frequencies for which the **resonance-rise corrections can be made** with fair accuracy. The performance of the instrument is therefore ratber considerably determined by the limitations of the tube itself, and further improve**ment in resonance-rise conditions would lead to only a minor increase in the use**ful frequency range. For this type of voltmeter, then, it would seem that the practical high-frequency limit with existing tubes had been approached closely.

The user must remember that in order to obtain the frequency characteristics **given in Figure 5, he must be very** careful when making connection to the probe. Thc rclationship bctween the voltage at thc probe terminals and the voltage that it is desired to measure at **some point in a circuit depends upon the** connections used. The voltage applied to the probe is that at its terminals, **which is not necessarily the same as** that at the far end of the connecting leads. At high frequencies the connection must be as short and direct as possible.

The three types of terminals supplied for usc with the probe are shown in Figure 4. They include a Type 274 plug terminal and Type 774 male and female coaxial terminals. A 50-ohm disc-type resistor is supplied for use with the **coaxial lerminals. 'The metal cap shown** directly in front of the probe is used to attach all terminals to the probe. There are three threaded holes around the edge of the cap instead of only the one **which is necessary for attachment of** the Type 274 plug low terminal. The three holes arc provided so that the cap can be fastened to a metal sheet or α other flat metal surface when a mini**mum ground-connection inductance** is desired. A hole in the metal sheet or surface makes the high probe input **terminal accessible.**

figure 7. Plot of impedance vs. frequency for the parallel components of input impedance. The equivalent parallel capacitance is $3.1 \mu\mu\text{f}$.

At frequencies low enough so that higher input capacitance and lower input natural frequency arc not *im*portant, the probe can be plugged into **position in the storage compartment and** the a-c voltage applied to the panel a-c **input terminals.**

The probe shell is equipped with a cylindrical shield that has an aperture through which the diode is accessible. When the shield is rotated until the aperture into the probe is closed, the probe is complctely shielded. A molded bakelite shell slips over the probe and is held in place by an insulated nut. The exposed metal at the front end of the probe is the only exposed part of the probe that can be at a d-c potential to ground. Connection to the d-c ampli**fier is made with a three-wire, shielded** cable about three feet long.

'Vhen voltage measurements arc made on electronic circuits, or, for that matter, on cireuits of any kind, the measuring device should disturb the circuit as little as possible. That is, the input impedance of the measuring device should be as high as possible. **A IOO-megohm resistor is shunted across** the diode rectifier and another 100 **megohm resistor is connected in series** with the lead from the diode plate to the grid of the d-c amplifier tube. These **resistance values give an effective** parallel input resistance of 25 megohms at low frequencies. At high frequencies **the input resistance is reduced by the** Boella effect' in the resistors and by

increased losses in the dielectrics. The input capacitance to the probe proper \mathbf{i} **s** about 3.1 micromicrofarads of which **0.8 micromicrofarad is the plate-to**cathode capacitance of the diode. When **the cap used for attaching the terminal::;** is screwed on the probe and the Type 274 plugs are used, the input capacitance **is increased about 1 micromicrofarad. Figure 6 shows curves of probe input resistance and input reactance versus frequency. 1'he input reactance curve is** calculated for an input capacitance of **3.1 mieromicrofarads.**

Amplifier

The bridge-type amplifier is shown in simplified form in Figure 8. The indi**cating meter is connected in series with the appropriate precision wire-wound** resistor between the cathodes of the twin-triode voltmeter tube, V-3. The cathodes of V-3 arc connected directly to the plates of V-4, another twin triode. The latter tube is used to provide high degeneration without using high **values of resistance from the cathodes** of V-3 to ground and, consequently, a high plate-supply voltage. Each triode **section of V-4, together with its cathode resistor, has the effect of a 7-megohm incremental resistance to voltage changes** from the cathode of V-3 to B-; yet the plate-supply voltage need be only 450 volts because of the low d-c drop in the

² Boella, M., ''Sul comportamento alle alta frequenze di
alcuni tipi di resistenze elevate usate nei radio-circuiti,''
Alta Frequenza, Vol. 3, p. 132, April 1934.

Figure 8. Elementary schematic circuit **diagram of the Type 1800-A Vucuum·Tube Voltmeter.**

tube. Since the incremental resistance from the V-3 eathodes to B- is high **compared to the resistance of the meter circuit, the amount of degeneration is** determined almost completely by the **meter-circuit resistance. At voltage** ranges of 15 volts full scale and higher, the degeneration is sufficient to prevent tube changes from affecting the calibration of the instrument. Controls are provided for adjusting the calibration of the 0.5, 1.5, and 5-volt a-c and d-c **ranges in case it is ever necessary to** change V-3. Change of any other tube except V-I, the diode rectifier, has no effect on the calibration. Changing V-I may require readjustment on the low **a-c ranges.**

Input to the voltmeter tube, V-3, for a-c or d-c measurements is selected by the combined power and selector switch mentioned previously. The d-c input system provides an R-C filter to prevent any ripple voltage from reaching V-3. The desired input resistance is obtained by proper connection of the short-circuiting link at the panel D-C input terminals. The input resistance of the OPEN GRID circuit is determined by the insulation resistance and the grid current which flows from V-3 through the voltage source. When the a-c input is selected, a diode, V-5, and circuit identical to that in the probe is connected to the grid of the inactive triode of V-3. The purpose of this diode is solely to balance the voltage developed at the other grid of V-3 from contact potentials and initial velocity of electrons in the probe diode. V-I and V-5 must be selected so that each tube gives approximately the same value of initial developed voltage. The heater current for the two diodes, V-I and V-5, is regulated with an Amperite 3-4 ballast lamp in order to maintain the **zero of the low voltage a-c ranges as** stable as possible.

Zero adjustment of the indicating meter is accomplished by adjusting the grid biases of V-3 very slightly. Bias adjustment is made on one grid to take care of large zero shifts such as may be encountered when V-3 is changed. Bias adjustment on the other grid, which should be sufficient for all normal adjustment necessary during actual use of the instrument, is made with the panel ZERO control. A third zero control is provided to adjust the a-c zero into coincidence with the d-c zero. The control varies the division of heater current between the two diodes, V-I and V-5, and so changes the initial voltage developed by each diode. Coincidence of the two zeros is of interest only for the sake of convenience. Lack of coincidence has no effect on the accuracy of **measurement. A change of resistance in** series with the indicating meter, which happens whenever the VOLTAGE RANGE switch is rotated, has no effect on the zero reading.

Power Supply

In order to maintain an accurate, stable meter reading on the low-voltage ranges, the plate supply voltage must be held constant regardless of power-line voltage fluctuations. Stabilization of the plate-supply voltage is obtained by use of an electronic voltage-stabilizing cir**cuit, consisting of two vacuum tubes** and two neon lamps. Both the shunt amplifier tube of the stabilizing circuit and the variable-resistance series tube are miniature types. The voltage across **two neon lamps in series is used as the** stable reference voltage of the system. When adjusted properly, the circuit maintains the plate-supply voltage within a volt or two of 450 volts as the power-

line voltage is varied from 105 to 125 volts. Heater voltage changes in all tubes except the two diodes, V-I and V-5, have no appreciable effect on the meter reading. The heater current of V-I and V-5 is, as mentioned above, regulated by a ballast lamp.

The controls used for calibration and **circuit adjustment are mounted on a** shelf at the bottom of the chassis where they are easily accessible when the **instrument is removed from its cabinet.** All of the circuit elements of the voltmeter except those in the prohe are mounted on the panel and a small, compact chassis. The chassis circuit elements and the panel circuit elements are connected together with a flexible cable so arranged that the panel and **chassis may be swung apart to allow** easy access to all portions of the circuit.

Figure 9 shows a view of the complete assembly and a view of the chassis and panel separated to expose all parts of **the circuit for servicing. The two** sec~ **tions arc separated by removing four screws and unsoldering two direct con**nections to the grids of the voltmeter tube, V-3.

The Type 1800-A Vacuum-Tube Voltmeter has many advantages over the older Type 726-A. It is smaller, lighter, **and easier to use ^j it can measure d-c** voltages; it is more stable against line**voltage changes; its input impedance is** higher and its frequency range is substantially greater. Mechanically and electrically, full advantage is taken of **modern techniques and new components** to produce an outstanding new volt**meter.**

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Figure 9. Two views of the chassis. At the right is shown the complete assembly, while the view at the left shows **how chassis ood ponel separate for servicing.**

SPECIFICATIONS

Voltage Range: 0.1 to 150 volts, a-c, in six ranges $(0.5, 1.5, 5, 15, 50, \text{ and } 150 \text{ volts}, \text{full scale})$; 0.01 to 150 volts, d-c, in six ranges (0.5, 1.5, 5, 15, 50, and 150 volts, full scale).

Accuracy: D-C, $\pm 2\%$ of full scale on all six ranges. A-C, $\pm 2\%$ of full scale on all six ranges for sinusoidal voltages.

Waveform Error: On the a-c voltage ranges, the instrument operates as a peak voltmeter calibrated to read r-m-s values of a sine wave, or 0.707 of the peak value of a complex wave. On distorted waveforms the percentage deviation of the reading from the r-m-s value may be as large as the percentage of harmonics present.

Frequency Error: At high frequencies resonance in the input circuit and transit-time effects in the diode rectifier introduce errors in the meter reading. The resonance effect causes the meter to read high and is independent of the applied voltage. The transit-time error is a function of the applied voltage and tends to cause the meter to read low. The curves of Figure 5 give the frequency correction for several different voltage levels. It will be noted that at low voltages the transit-time and resonance effects tend to cancel, while at higher voltages the error is almost entirely due to resonance.

This voltmeter may be used at frequencies as low as 20 cycles with a frequency error of less than 2% .

Input Impedance: At low frequencies the equivalent parallel resistance of the a-c input circuit is 25

megohms. At higher frequencies this resistance is reduced by losses in the shunt capacitance. The equivalent parallel capacitance at radio frequencies is $3.1 \mu \mu f$ with the probe cap and plug removed. At audio frequencies this capacitance increases slightly. The probe cap and plug add approximately $1\mu\mu f.$ The accompanying plot gives the variation of R_p and X_p with frequency.

On the d-c ranges two values of input resistance are provided, 10 megohms and open grid.

Power Supply: 105 to 125 volts or 210 to 250 volts, a-c, 50 to 60 cycles. The instrument incorporates a voltage regulator to compensate for supply variations over this voltage range. The power input is less than 25 watts.

Tubes: Two TYPE 9005, two TYPE 6SL7-GT, one TYPE 6AT6, one TYPE 6C4, one TYPE 6X5-GT, one TYPE 3-4, and two TYPE 991 are used; all are supplied.

Accessories Supplied: A seven-foot line connector cord, spare meter lamps and fuses; TYPE 274 and TYPE 774 terminations and 50-ohm terminating resistor for probe.

Mounting: Black crackle finish aluminum panel mounted in a shielded walnut cabinet. The carrying handle can be set as a convenient support for the instrument when placed on a bench with the panel tilted back.

 $\textbf{Dimensions:}$ (Width) $7\frac{3}{8}''$ x (depth) $7\frac{1}{2}''$ x (height) $11\frac{1}{8}''$, over-all.

Net Weight: 13 pounds.

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