



IMPROVED PERFORMANCE FROM THE UNIT PULSE GENERATOR

One of our most popular Unit Instruments has long been the TYPE 1217 Unit Pulse Generator. The reason for its popularity is easy to see: It has consistently offered more prf range, pulse duration, and pulse amplitude per dollar than any other instrument of its type. Now, with the introduction of the TYPE 1217-C Unit Pulse Generator, specifications have been again improved significantly. The size remains the same, and the performance per dollar has again been sharply boosted, to a point where the Unit Pulse Generator is a model of value engineering.

For those who are familiar with

earlier models of the TYPE 1217, the major improvements in performance are: increased prf to 1.2 Mc/s (internal drive) and 2.4 Mc/s (external drive), and improved transition times to less than 10 nanoseconds with a more symmetrical pulse (see Figure 2).

For those who are unfamiliar with the Unit Pulse Generator, it is a compact, general-purpose pulse source, whose prf can be either internally controlled from 2.5 c/s to 1.2 Mc/s or externally controlled (the input circuits are then arranged as an aperiodic switching circuit) from dc to 2.4 Mc/s. Pulse duration is adjustable from 100 nanoseconds to 1.1 seconds, and ampli-



Figure 1. Type 1217-C Unit Pulse Generator with power supply.

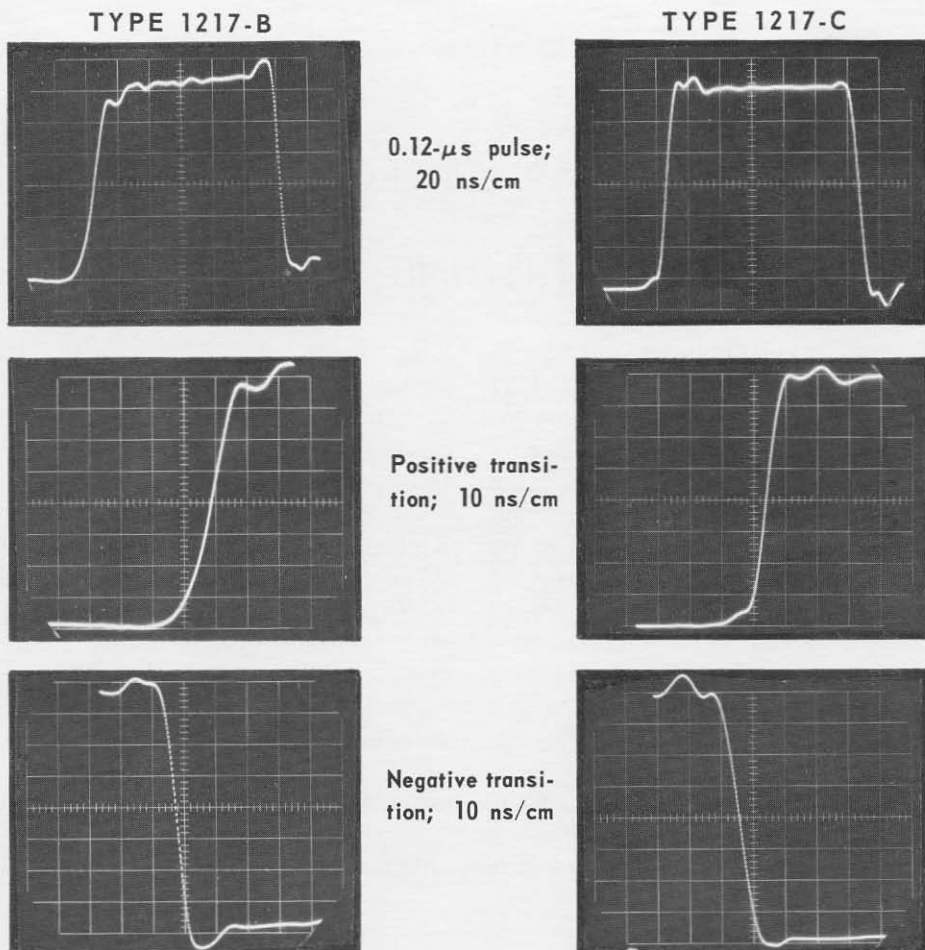


Figure 2. Oscilloscope showing improvements in pulse symmetry and rise times in Type 1217-C over its predecessor.

tude of the 40-mA output pulse is also adjustable, up to 40 volts, peak (the AMPLITUDE control is actually calibrated in output impedance). Positive and negative prepulses and a delayed synchronizing pulse are also provided.

The Circuit

The circuit is basically that described in an earlier article on the TYPE 1217-B¹; a block diagram is shown in Figure 3.

A major design objective was economy, and this meant making every circuit component work all the time and to its full capability. The internal prf oscillator uses the same parts — rearranged by switching — that make up the input circuits in the external-drive mode. Another design feature was the com-

¹ R. W. Frank, "More and Better Pulses from the Unit Pulse Generator," *General Radio Experimenter*, 36, 1-2, January-February 1962.

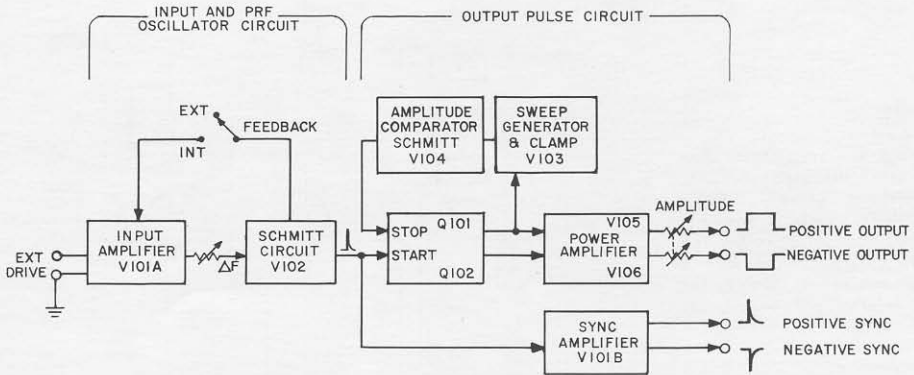


Figure 3. Block diagram.

mon-sense utilization of tubes and transistors to exploit the strong points of both.

The main components of the pulse generator are an input system, a pulse-timing circuit, and a power amplifier. Switched for internal control of prf, the input system is a stable, wide-frequency-range oscillator. Switched for external control, the circuit becomes an aperiodic trigger generator, made up of a de amplifier and a Schmitt trigger. This circuit produces a single, brief, trigger pulse to initiate the action of the pulse-timing circuits once for each cycle of the input driving signal.

The output circuits include a set-reset bistable circuit, an RC ramp generator, and an amplitude comparator.

The circuit is similar to that used in all precision pulse generators and makes possible a relatively linear pulse-duration dial scale, low jitter, quick recovery time, and operation highly independent of supply-voltage changes and aging of the active devices. The warmup effects on prf and on pulse duration are shown in Figures 4 and 5.

The set-reset bistable circuit drives a pair of output tubes, which apply current to variable load resistors. The maximum value of these resistors is 1000 ohms, and the output current is over 40 mA; the maximum output voltage is therefore at least 40 volts.

The delayed (synchronizing) pulse corresponds to the late transition of the output pulse. This delayed pulse

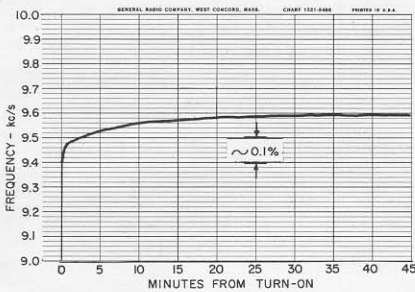


Figure 4. Warmup effects on pulse repetition frequency.

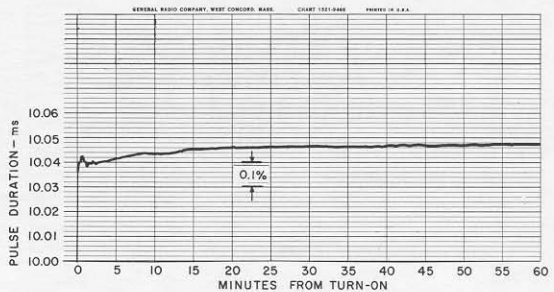
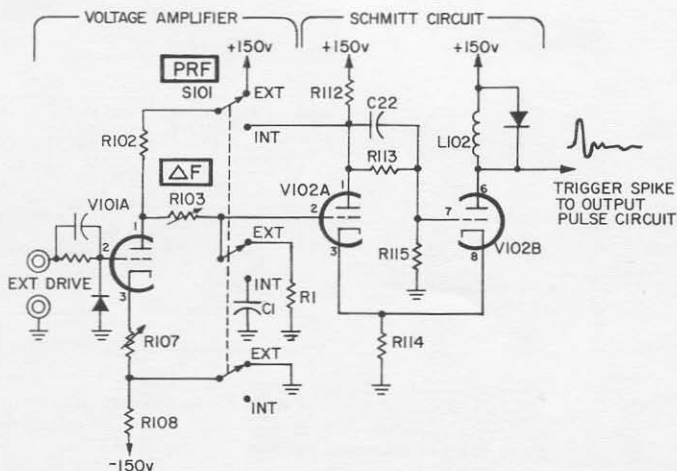


Figure 5. Warmup effects on pulse duration.



Figure 6. Schematic diagram of the input circuits. Switching at only three points converts a conventional Schmitt circuit, used with external drive, into a wide-range oscillator for internal prf control.



can be used to drive a second pulse generator; a pair of pulse generators therefore makes an excellent delayed-pulse generator, and three make a good double-pulse generator.

Output Pulse Waveform

The improvement in pulse transition time and symmetry comes about from the use of silicon transistors in place of germanium units. The voltage wave-

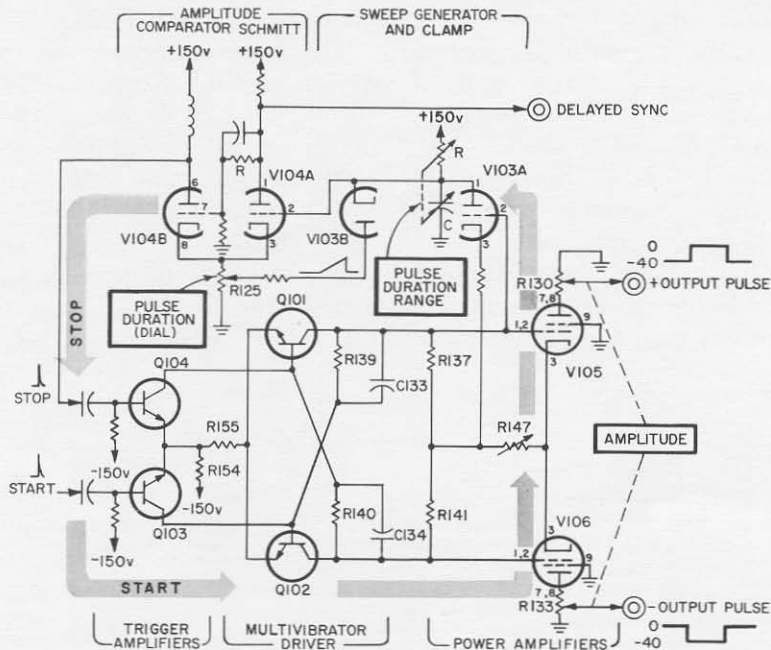


Figure 7. Schematic diagram of timing and output circuits. Transistors Q101 and Q102 are connected in a bistable circuit to control conduction of the output power tubes, V105 and V106. Such hybrid design exploits strong points of both tubes and transistors.



form at the output terminals depends on the termination. In Figure 2, the terminating resistance is 50 ohms. All transition times are less than 10 nanoseconds, and some overshoots occur. With no external loading, the very fast current transitions are applied to the 1000-ohm output potentiometer and an inherent stray capacitance of about 30 picofarads, and the voltage rise time is about 60 nanoseconds. Externally add-

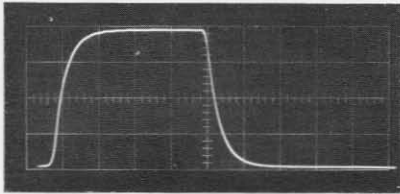
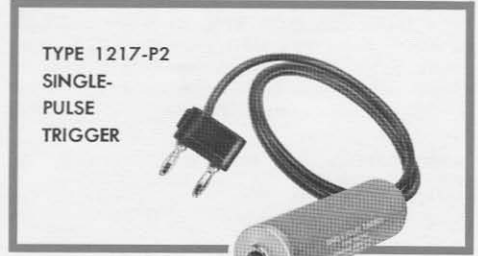


Figure 8. Oscillogram showing effects of 12-pF probe on output pulse.

ed capacitance will increase this rise time by about 2 nanoseconds per picofarad. With this output configuration, no overshoot occurs, and the rise is purely exponential (see Figure 8).

Pulse DC Component

Notice, in Figure 7, that a dc component negative with respect to chassis ground appears on both the positive and negative pulses. When the amplitude control is fully open, the positive pulse rises from -40 volts to ground, and the negative pulse falls from ground to -40 volts. In other words, only the



negative output is truly "ground-based."

In many applications, the output will be capacitively coupled, and the dc component of the pulse will be of no consequence. Even when the dc component is important, however, it is rarely necessary that the positive pulse start precisely from chassis ground. In most cases it is desirable that the pulses make a transition from a potential other than ground. Adjustment at this potential is easy to accomplish. Figure 9 shows a simple method of voltage translation by which the dc level of either a positive or negative pulse can be adjusted as desired. A 400-volt laboratory power supply can thus translate the positive pulse so that it is completely above ground, with only a 10-percent reduction in output impedance. In most applications, no such power need be wasted for dc translation. Pulse amplifiers, "and" gates, etc, can be biased directly from the pulse gen-

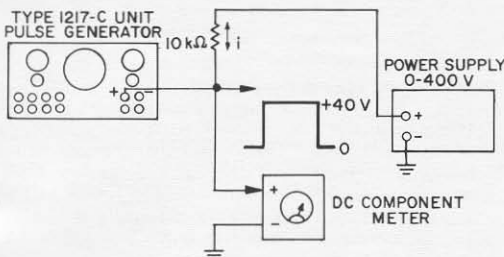


Figure 9. Connection of 400-V laboratory power supply and dc voltmeter for full translation of positive pulse. Any desired dc component can be obtained by adjustment of power-supply voltage. Dc component meter can be used to indicate duty ratio.

Figure 10. Control of transistor switching by Unit Pulse Generator. (top) NPN, normally on, goes off during pulse time. NPN, normally off, goes on during pulse time. PNP, normally off, goes on during pulse time. PNP, normally on, goes off during pulse time.

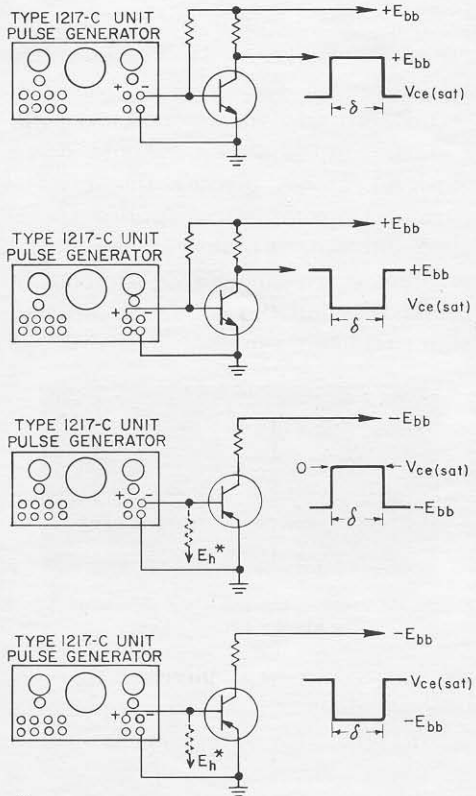
erator with low-power networks, as shown in Figure 10.

Uses

The TYPE 1217-C Unit Pulse Generator is a valuable tool in any laboratory where pulses are used. Its generalized characteristics and low price make it an ideal instrument for school-laboratory experiments in pulse techniques, as well as for work on radar, pulse communication, and computer systems.

Experience has also shown that the pulse generator is a useful source for measurements on transistor systems. It can operate saturated transistor switches, both npn and pnp, without coupling networks (see Figure 10). Since the pulse generator is direct-coupled, the solid-state switches can be operated over its full duration range.

— R. W. FRANK



SPECIFICATIONS

PULSE REPETITION FREQUENCY

Internally Generated: 2.5 c/s to 1.2 Mc/s, with calibrated points in a 1-3 sequence from 10 c/s to 300 kc/s, and 1.2 Mc/s, all $\pm 5\%$. Continuous coverage with an uncalibrated control.

Externally Controlled: Aperiodic, dc to 2.4 Mc/s with 1 V, rms, input (0.5 V at 1 Mc/s and lower); input impedance at 0.5 V, rms, approximately 100 k Ω shunted by 50 pF. Output pulse is started by negative-going input transition.

OUTPUT-PULSE CHARACTERISTICS

Duration: 100 ns to 1 s in 7 decade ranges, $\pm 5\%$ of reading or $\pm 2\%$ of full scale or ± 35 ns, whichever is greater.

Rise and Fall Times: Less than 10 ns into 50 or 100 Ω ; typically 60 ns + 2 ns/pF external load capacitance into 1 k Ω (40 V).

Voltage: Positive and negative 40-mA current pulses available simultaneously. Dc coupled, dc component negative with respect to ground. 40 V, peak, into 1-k Ω internal load impedance for both negative and positive pulses. Output

control marked in approximate output impedance.

Overshoot: Overshoot and noise in pulse, less than 10% of amplitude in correctly terminated measuring system.

Ramp-off: Less than 1%.

Synchronizing Pulses:

Pre-pulse: Positive and negative 8-V pulses of 150-ns duration. If positive sync terminal is shorted, negative pulse can be increased to 50 V. Sync-pulse source impedance:

- positive — approx 300 Ω ;
- negative — approx 1 k Ω .

Delayed Sync Pulse: Consists of a negative-going transition of approximately 5 V and 100-ns duration coincident with the late edge of the main pulse. Duration control reads time between prepulse and delayed sync pulse. This negative transition is immediately followed by a positive transition of approximately 5 V and 150 ns to reset the input circuits of a following pulse generator. (See oscillogram.)



Stability: Prf and pulse-duration jitter are dependent on power-supply ripple and regulation. With TYPE 1201 Power Supply, external-drive terminals short-circuited, prf jitter and pulse-duration jitter are each 0.01%. With TYPE 1203 Power Supply, they are 0.05% and 0.03%, respectively. (Jitter figures may vary

somewhat with range switch settings, magnetic fields, etc.)

GENERAL

Power Required: 300 V at 60 mA, 6.3 V at 3 A. Type 1203 Unit Power Supply or Type 1201 Unit Regulated Power Supply is recommended.

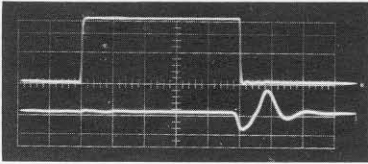
Accessories Available: TYPE 1217-P2 Single-Pulse Trigger, rack-adaptor panel for both generator and power supply, 19 by 7 in (485, 180 mm).

Cabinet: Unit-Instrument type.

Dimensions: Width 10 3/4 (15 with power supply), height 5 3/4, depth 6 1/2 inches (275, 150, 165 mm), over-all. Rack-adaptor panel, 19 by 7 inches (485, 180 mm).

Net Weight: 4 1/2 lb (2.1 kg).

Shipping Weight: 6 lb (2.8 kg).



1- μ s pulse into 50 ohms with delayed sync pulse.

Type		Price
1217-C	Unit Pulse Generator	\$275.00
1217-P2	Single-Pulse Trigger	25.00
1203-B	Unit Power Supply (for 115-volt supply)	55.00
1203-BQ18	Unit Power Supply (for 230-volt supply)	60.00
480-P4U3	Relay-Rack Adaptor Panel	12.00



A RECIPROCITY CALIBRATOR
FOR THE
WE 640AA AND
OTHER MICROPHONES

Among the great time savers of recent invention was the GR TYPE 1559-A Microphone Reciprocity Calibrator¹, which replaced the tedium of a long, meticulous laboratory calibration with a minute or two of knob turning. The

original model, however, accepted only the General Radio measurement microphone, a limitation overcome by the new TYPE 1559-B Microphone Reciprocity Calibrator. Of especial importance is the fact that the new model will also calibrate the Western Electric 640AA-type microphone. Since the Na-

¹Basil A. Bonk, "Absolute Calibration of PZT Microphones," *General Radio Experimenter*, 37, 4-5, April-May 1963.